

9th Chemical Process Safety Sharing (CPSS)

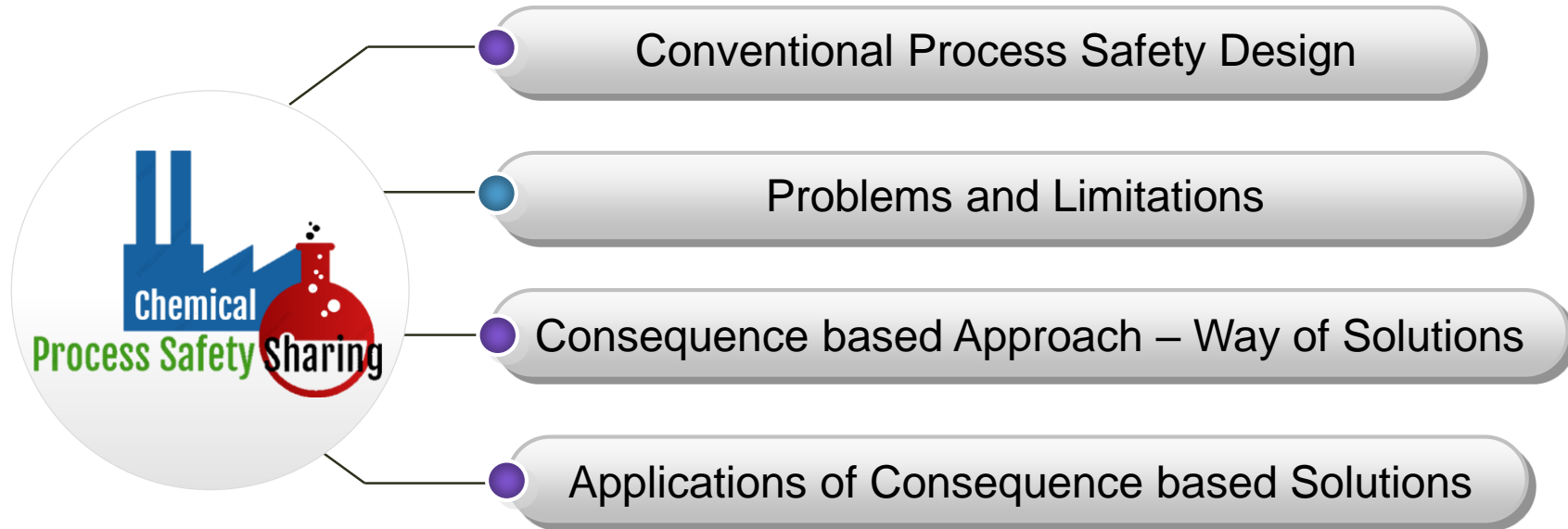
Consequence based Solutions for Process Safety Engineering Design

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Contents



Conventional Process Safety Design



Design on context based references in accordance with the following order of precedence;

- I. Country Laws and Regulations
- II. International Codes and Standards
- III. Company Standards
- IV. General Best Practices/Guidelines
- V. Internal/External Lessen Learns

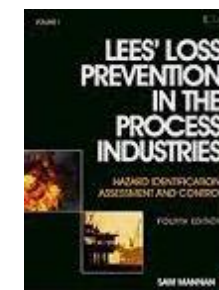
Conduct PHA study to assist the design

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GE GAP Guidelines





Problems and Limitations



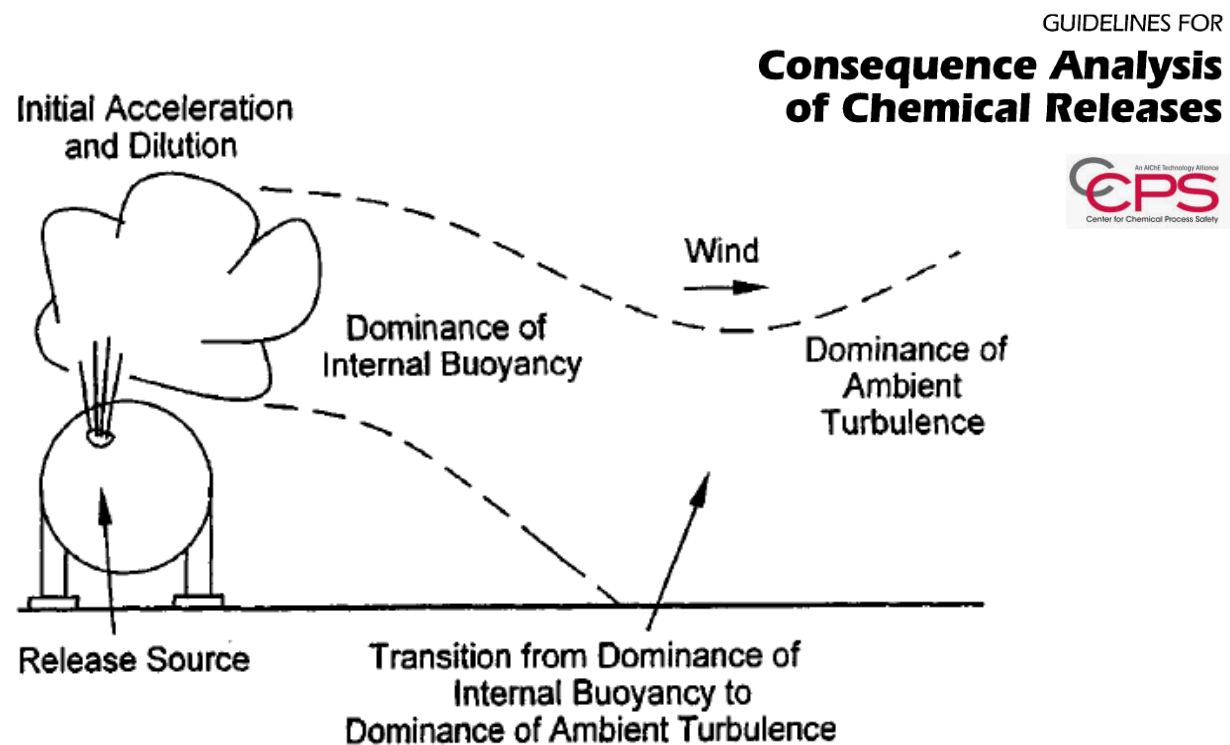
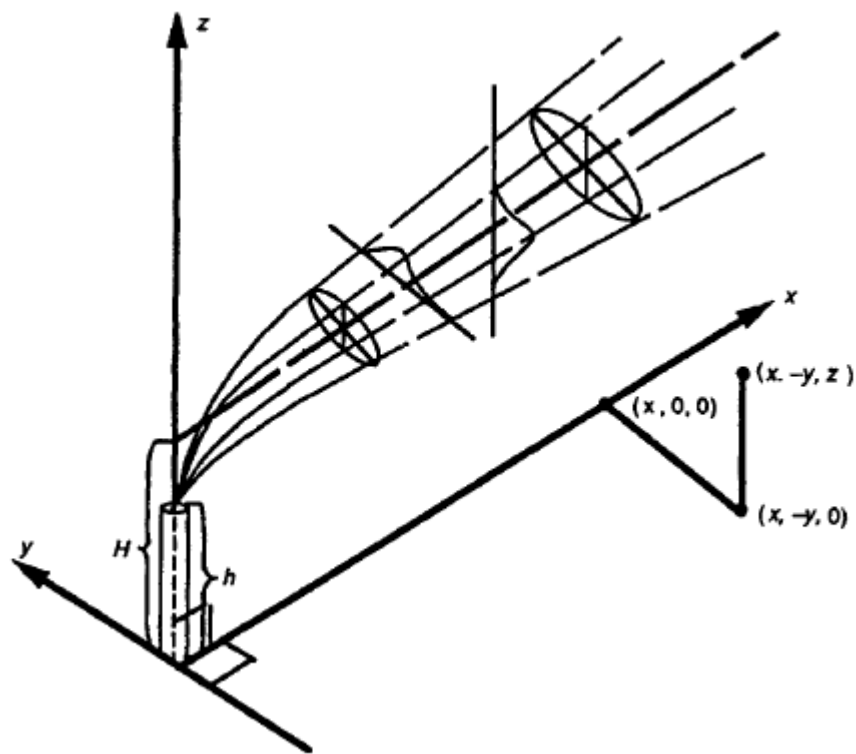
There are pain points facing when we design under context references based;

- Unable to implement
- Over design (over budget)
- Under design (ensure safe?)
- Unclear
- Too general
- Not define/Not relate

Consequence based Approach – Way of Solutions



Apply the physical effect model by consequence modeling tool(s) to quantify the hazard impact i.e. dispersion, fire and explosion to solve engineering design problems

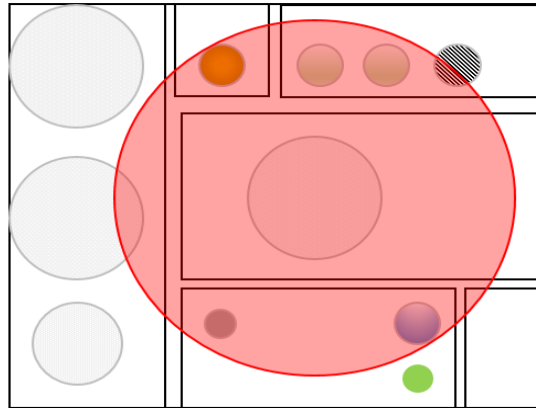


Consequence based Approach – Benefits



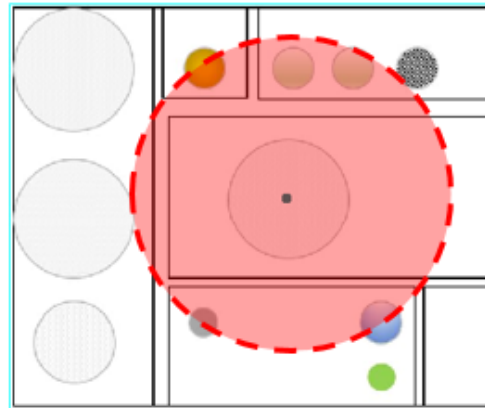
Offer effective solutions and optimum safety design

e.g. Limit firefighting resource for spray cooling



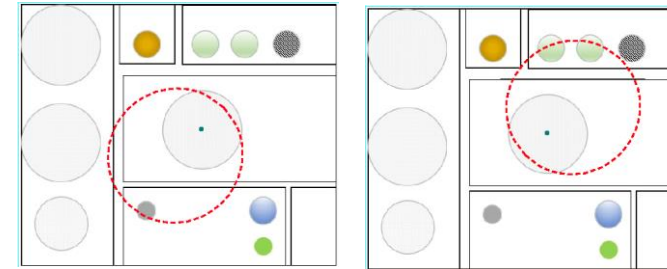
1-dia of burning tank (NFPA30) needs exposure protection.

Code based

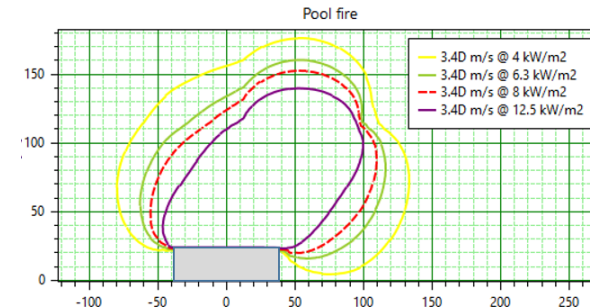


Ambient wind, radius is 91% of 1-dia burning tank

Consequence based



Standalone Pool Fire Radiation on a Plane



- Person pain after 20 s (world bank)
- Max heat limit for fire responder (IP19)
- Fire escalation if long exposure & no protection (IP19)
- Safe operating maximum for steel structure & process equipment with no protection (API2218)



Consequence based Approach – Suggestions



Select the right consequence modeling tool(s)

- Validated and technically proved math model for the hazard scenario studied
- Known features and appropriate use of each model for the hazard scenario
- Known limitations of those consequence modeling tool(s)



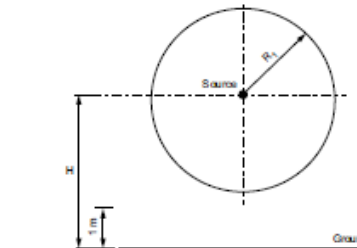
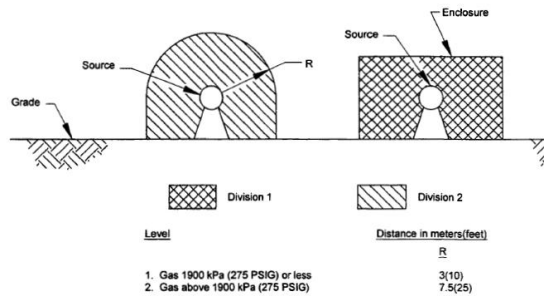
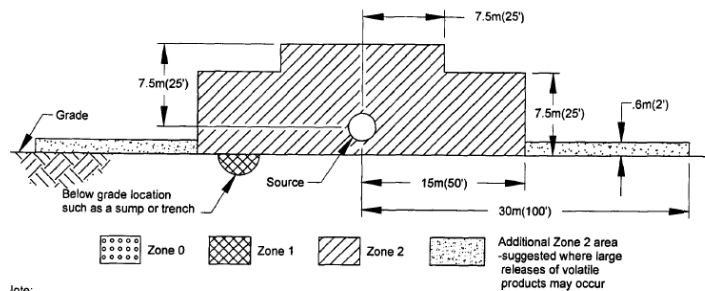
Select the reliable impact criteria source(s)

- Dispersion (flammable/toxic) impact
- Fire (Thermal) impact
- Explosion (Overpressure) impact

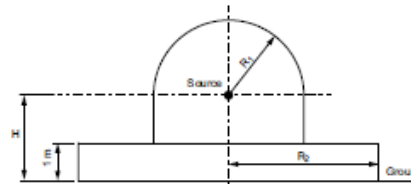


Hazardous Area Classification

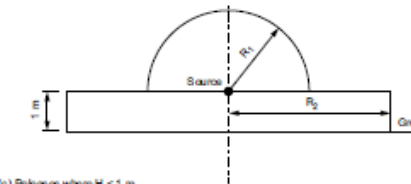
Code based → API500/505, NFPA 497, IE(IP) 15



(a) Releases where $H > R_1 + 1\text{ m}$



(b) Releases where $1\text{ m} < H < R_1 + 1\text{ m}$

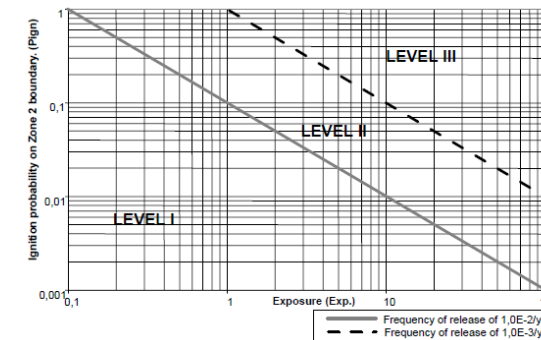


(c) Releases where $H < 1\text{ m}$

Table 5.3 Example calculation for compressors – leak hole size and hazard radius (R_1)

Release frequency	Seal type	Release hole diameter (mm)	Hazard radius R_1 (m)	
			G(I)	G(II)
LEVEL I	Floating ring	5	4	6
	Purged labyrinth	12	10	13
LEVEL II	N/A	22	†	†
LEVEL III	N/A	70	†	†

N/A Not applicable since hole size is independent of seal type.
 † These hole sizes are considered greater than should be used for hazardous area classification purposes. This Code does not therefore give hazard radii for these hole sizes. The user may determine the hazard radii by calculation.



Individual Risk (/yr) from a number of ignited secondary grade release sources is defined as:

$$IR_{\text{Ignited release}} (/yr) = F_{\text{dam}} / (\text{release source-yr}) * P_{\text{ign}} * P_{\text{occ}} * V * N_{\text{range}}$$

Direct example

Point source/Risk-based

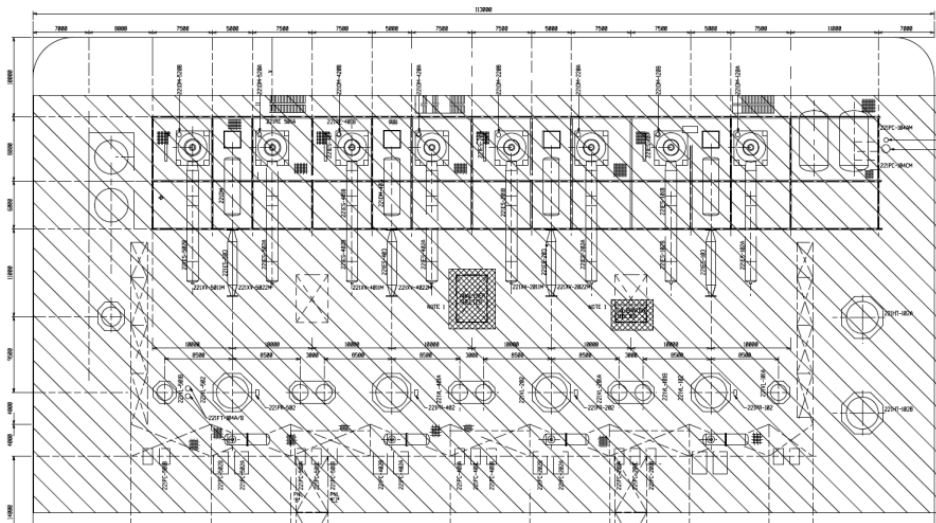
Applications of Consequence based Solutions



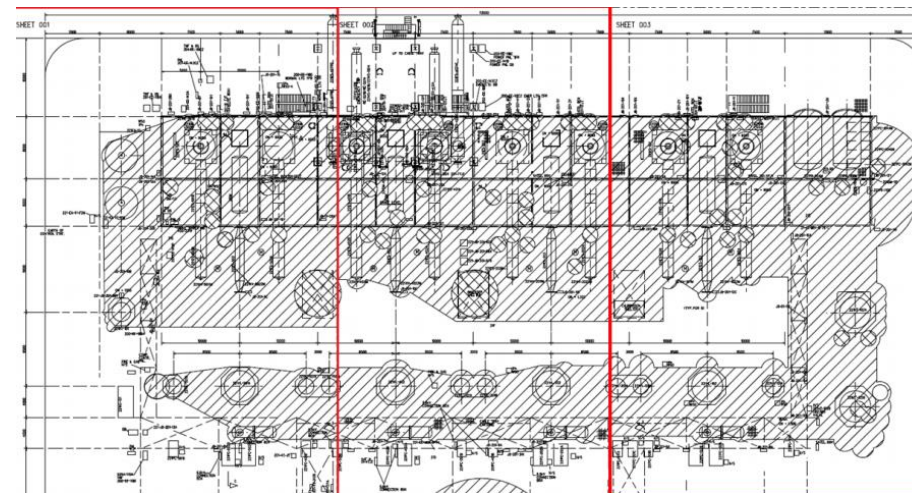
Hazardous Area Classification

Code based → API500/505, NFPA 497, IE(IP) 15

Scientific and lower budget !!!



Direct example



Point source/Risk-based

Applications of Consequence based Solutions



Hazardous Area Classification

Code based → Point source/risk based

Conduct dispersion modeling

Not applicable for chemical plants !!!

Reference may not reflect to real conditions !!!

Stream component (mol %)	Fluid category					LFL (vol %)	Molecular weight (g/mol)	Boiling point (°C)
	A	B	C	G(i)	G(ii)			
N ₂ Nitrogen	0,00	0,00	0,00	2,00	2,00	-	28,01	-196
C ₁ Methane	0,00	4,00	0,00	88,45	10,00	5,00	16,04	-161
C ₂ Ethane	0,00	0,00	0,00	4,50	3,00	3,00	30,07	-87
C ₃ Propane	70,00	6,00	1,00	3,00	3,00	2,10	44,09	-42
C ₄ Butane	30,00	7,00	1,00	100	1,00	1,80	58,12	-1
C ₅ Pentane	0,00	9,00	2,00	1,00	0,00	1,40	72,15	36
C ₆ Hexane	0,00	11,00	3,00	0,00	0,00	1,20	86,17	69
C ₇ Heptane	0,00	16,00	3,00	0,00	0,00	1,05	100,20	98
C ₈ Octane	0,00	22,00	27,00	0,00	0,00	0,95	114,23	126
C ₉ Nonane	0,00	0,00	25,00	0,00	0,00	0,85	128,26	151
C ₁₀ Decane	0,00	25,00	38,00	0,00	0,00	0,75	142,28	173
H ₂ O Water	0,00	0,00	0,00	0,05	0,00	-	18,02	100
Carbon dioxide	0,00	0,00	0,00	0,00	1,00	-	44,01	-78
Hydrogen	0,00	0,00	0,00	0,00	80,00	4,00	2,02	-253
Average MW (g/mol)	48,30	100,06	125,03	18,74	7,03			
LFL (vol %)	2,00	1,05	0,86	4,6	4,00			
LFL (kg/m ³)	0,039	0,042	0,043	0,034	0,011			

Table C2: Physical parameters used in dispersion modelling

Parameter	Value used in EI15
Ambient temperature	30 °C ✓
Storage/process temperature	20 °C
Relative humidity	70 % ✓
Wind speed	2 m/s ✓
Stability class	D
Surface roughness length	0,03 m
Release direction	Horizontal
Release height	For R ₁ : 5 m For R ₂ : 1 m
Release angle	For R ₁ : horizontal For R ₂ : unknown
Sample time	18,75 s
Reference height	10 m
Hazard distances	To LFL

The dispersion modelling contained in *EI Research Report: Dispersion modelling and calculations in support of EI Model code of safe practice – Part 15: Area classification code for installations handling flammable fluids* was carried out using DNV PHAST. The results were sufficiently consistent with those in the previous edition of this Model Code² to support using DNV PHAST without modifying the standard approach to modelling these releases.



Plant layout and sitting

Topic	Impact Criteria for design parameter	
	Unit	Description
Thermal Radiation Level impact on equipment unit	12.5 kW/m ²	Glazed building impairment
	37.5 kW/m ²	Complete failure of the structure or significant damage to wall or roof
	250 kW/m ²	Structural steel and reinforced concrete framed building initiated failure and up to 30 minute impingement lead to total failure
	35 kW/m ²	Failure on building with combustible materials i.e. wood paneling
	25 kW/m ²	Failure on building with soft paneling i.e. porta cabin
Thermal Radiation Level impact on manned occupancy	4 kW/m ²	working area (personnel starting pain/injury)
Explosion Overpressure Level impact on building	<0.02 barg	No damage: Potential damage to window glass but no structural damage
	0.02-0.07 barg	For glazing and lightweight structures building : <ul style="list-style-type: none"> Large windows shatter at 0.03-0.069 bar, At 0.069 bar corrugated asbestos shatters/fastenings on corrugated steel or aluminum panels fail, Minor damage to house structure at 0.048 bar

Topic	Impact Criteria for design parameter	
	Unit	Description
Location for non-rated (no-ex-proof) electrical equipment	100%LFL	Located away from this contour coverage plus xxx m margin.
Location for equipment creating source of ignition (i.e. hot surface, open flame)	100%LFL	Located away from this contour coverage plus xxx m margin.

Quantify the possible hazard impacts of facilities

Conduct dispersion, fire & explosion modeling

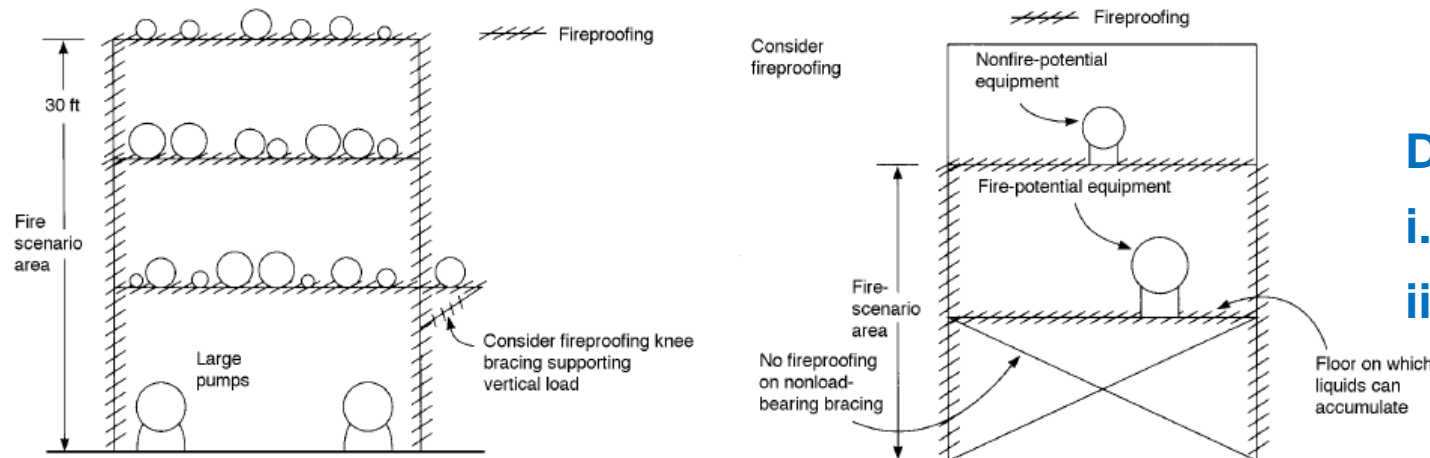


Fire proof design for building structure

Equipment	Protection Level ^a	Section in API 2218 or Other Reference
LPG vessels if not protected by fixed water spray systems.	Fireproofed equivalent to 1 ½ hours in UL 1709 (or functional equivalent).	API 2510 (1995) Section 8.7 Section 6.2.2
Pipe supports within 50 ft or in spill containment area of LPG vessels, whichever is greater.	Fireproofed equivalent to 1 ½ hours in UL 1709 (or functional equivalent).	Sections 6.2.2 and 6.2.3 API 2510 (1995) Section 8.8.5
Critical wiring and control systems.	15-to-30-minute protection in UL 1709 (or functional equivalent) temperature conditions.	Section 6.1.8.1 API 2510 (1995) Section 8.11

Note: ^aSome company standards require protection greater than that shown in column 2.

Over-design or Under-design ?



Conduct fire modeling

Determine

- i. The contour of thermal impact
- ii. How long does the burning last ?



Firewater supply duration

▪ NFPA 15

A.4.4.8 It is desirable to contain runoff for the anticipated duration of any fire. However, in large chemical or petrochemical facilities, a major fire can last for 8 hours or more, resulting in extremely large holding basins or retention ponds. Where the anticipated incident duration results in retention basins that are of impractical size, methods to limit the duration of runoff might be required.

When an extended duration is anticipated, a duration of 4 hours is usually considered the practical maximum. During that time, it is often possible to isolate equipment and reduce the flow rate of water and other materials so that the continuous discharge flow rate is less than the initial flow rate. If a significant amount of flammable materials can be removed from the protected area, it could be possible to shut down water spray systems and manually fight the fire, greatly reducing the amount of material that needs to be contained.

▪ CCPS (AIChE)

7.4.1.2. Tanks and Reservoirs

Limited capacity sources such as tanks and reservoirs can be provided as a source of water. The designs of tanks and reservoirs should be for the minimum judged necessary for fighting fire within the facility. This may be as little as a two hour supply for a relatively low risk plant, but a minimum of 4 hours is typical, based on the largest fire water demand. Within a facility, there may be certain units that require more than a four hour supply, i.e. due to a larger inventory of flammable materials. In such cases, additional sources of fire water will be required. This may mean temporary hook-up of a neighbor's system, use of cooling water, storm impoundment ponds, or reliance on municipal systems. A larger capacity may be warranted for larger and more complex facilities. Fire water pump suction tanks should be on ground level. Freeze protection should

Too general ?



Applications of Consequence based Solutions



Firewater supply duration



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พ.ศ. ๒๕๕๒

หมวด ๔

ระบบน้ำดับเพลิง

ข้อ ๑๐ ผู้ประกอบกิจการโรงงานต้องจัดเตรียมน้ำสำหรับดับเพลิงในปริมาณที่เพียงพอที่จะส่งจ่ายน้ำให้กับอุปกรณ์ฉีดน้ำดับเพลิงได้อย่างต่อเนื่องเป็นเวลาไม่น้อยกว่าสามสิบนาที

Not specific !!!

▪ API 2030

areas can be based on the potential fire exposure, the expected fire duration and drainage capacity. If process equipment cannot be isolated and de-inventoried quickly a fire can have a duration longer than the 1 to 4 hours protection that passive fireproofing can reasonably provide. Application of cooling water from spray systems (or firewater monitors or hand lines) should be given consideration in such cases since this can provide continuing protection for as long as the water supply lasts.

Conduct fire modeling

Assist to determine;

How long does the fire burning possibly last ?



Fire/Smoke & Gas Detectors mapping study

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หมวด ๒
ระบบสัญญาณแจ้งเหตุเพลิงไหม้

ข้อ ๔ อาคารโรงงานต้องจัดให้มีอุปกรณ์ตรวจจับและแจ้งเหตุเพลิงไหม้ครอบคลุมทั่วทั้งอาคารตามความเหมาะสมกับสภาพพื้นที่ โดยเฉพาะในพื้นที่ที่ไม่มีคนงานปฏิบัติงานประจำและมีการติดตั้งหรือใช้งานอุปกรณ์ไฟฟ้า หรือจัดเก็บวัสดุไวไฟหรือวัสดุติดไฟได้ง่ายจะต้องติดตั้งอุปกรณ์ตรวจจับและแจ้งเหตุเพลิงไหม้อัตโนมัติ

Not define !!!

Conduct dispersion & fire/smoke(CFD) modeling

17.8.3.2 Spacing Considerations for Flame Detectors.

17.8.3.2.1* The location and spacing of detectors shall be the result of an engineering evaluation that includes the following:

- (1) Size of the fire that is to be detected
- (2) Fuel involved
- (3) Sensitivity of the detector
- (4) Field of view of the detector
- (5) Distance between the fire and the detector
- (6) Radiant energy absorption of the atmosphere
- (7) Presence of extraneous sources of radiant emissions
- (8) Purpose of the detection system
- (9) Response time required

▪ NFPA 72

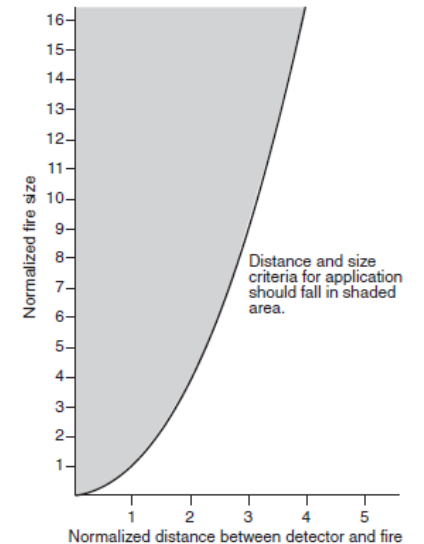


FIGURE A.17.8.3.1.1 Normalized Fire Size vs. Distance.



Q & A



9th Chemical Process Safety Sharing (CPSS)
9th Jun. 2022, Thailand





Thank you for your attention